

# LIGHTNING THREAT TO ABOVE GROUND AND BELOW GROUND STRUCTURES

## MODELING AND TESTING

~~500~~ 3 trillions FPK  
computations &  
simulate yrs  
of ltr.

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ANALYSIS AND TESTING

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# **LIGHTNING THREAT TO ABOVE GROUND AND BELOW GROUND STRUCTURES**

## **A. DIRECT THREAT**

- RESISTIVE HEATING OF CRITICAL ASSET ELEMENTS**
- [E.G. HUMANS . EXPLOSIVES, ELECTRICAL CIRCUITS]**
- DUE TO DIRECT ATTACHMENT OF LIGHTNING CURRENT**
- [INCLUDING POSSIBLE LIGHTNING SIDE FLASH AND/OR CURRENT SPLITS AT VARIOUS CONDUCTING JUNCTIONS]**

## **B. INDIRECT THREAT**

- RESISTIVE HEATING OF CRITICAL ASSET ELEMENTS**
- DUE TO INDIRECT SECONDARY CURRENTS INDUCED BY TIME VARYING ELECTRIC AND MAGNETIC FIELDS IN THE LIGHTNING ENVIRONMENT [ACTION AT A DISTANCE]**
- [INCLUDES POSSIBLE CAPACITIVE BREAKDOWN NEAR CLOSELY SPACED CONDUCTIVE ELEMENTS]**

## **C. RESONANCE COUPLING**

- RESONANCE COUPLING TO CRITICAL ASSETS IN THE LIGHTNING SPECTRAL RANGE – UP TO 20 OR 30 MHZ.**
- LONGER TERM HEATING OF CRITICAL ELEMENTS OVER SUCCESSIVE RESONANCE CYCLES**

# **LIGHTNING THREAT TO ABOVE GROUND AND BELOW GROUND STRUCTURES**

## **TEST METHODS**

### **A. ROCKET TRIGGERED LIGHTNING**

#### **EXAMPLES:**

**GAINSVILLE FLORIDA: ABOVE GROUND STRUCTURES  
FT. McCLELLAN: UNDERGROUND STORAGE BUNKERS**

### **B. HIGH VOLTAGE MARX GENERATORS**

#### **EXAMPLES:**

**FLORIDA: SPACE SHUTTLE LAUNCH PAD  
UTAH THIOKOL: SOLID ROCKET RAILCAR COVERS  
PITTSFIELD: LABORATORY SCALE MODELS**

### **C. LOW LEVEL RF CURRENT INJECTION**

**SINGLE FREQUENCY AT VARIOUS INJECTION POINTS  
-SWEPT OVER THE SPECTRAL RANGE OF LIGHTNING  
STRIKES UP TO 30 MHZ – MONITORED AT TEST POINTS  
-MANY EXAMPLES OF ABOVE GOUND AND BELOW  
GROUND STRUCTURES AND FACILITIES**

# RADIO FREQUENCY (RF) TESTING – EXAMPLES

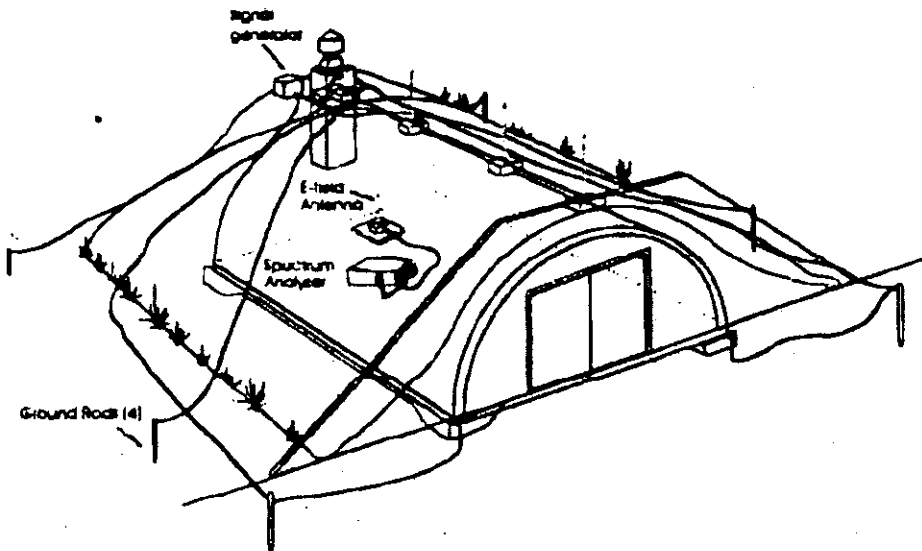
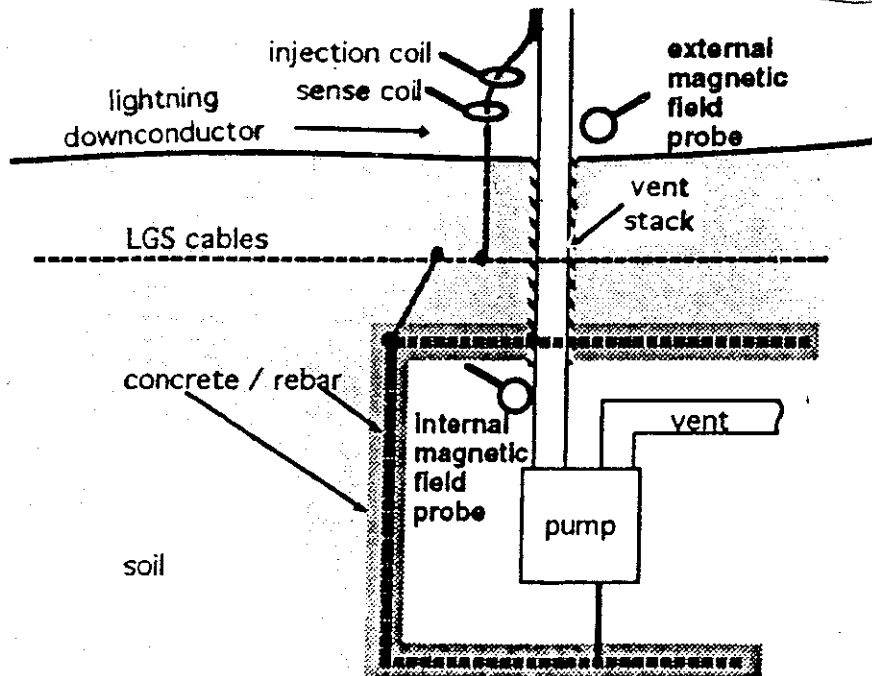


Figure 2. Typical equipment layout during transfer impedance testing.

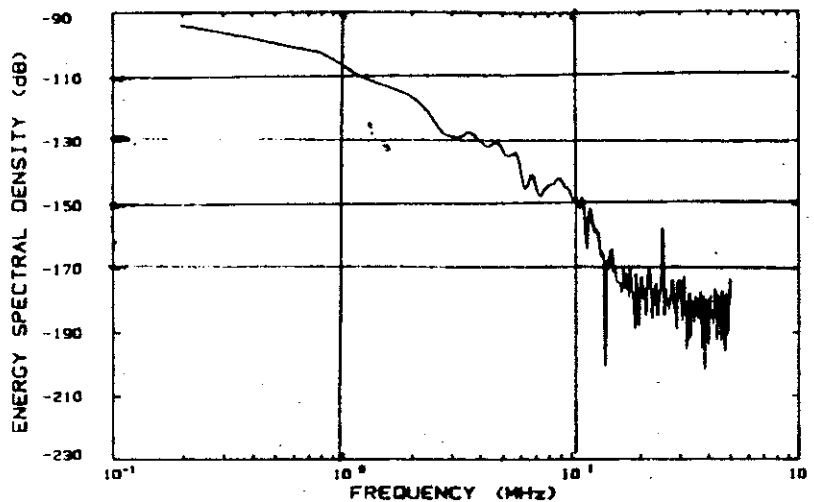
## GLOBAL TESTING – SHIELDING EFFECTIVENESS EXTERNAL VOLTAGE INJECTION



## LOCAL TESTING – PENETRATION/BOND CURRENTS EXTERNAL (OR INTERNAL) CURRENT INJECTION

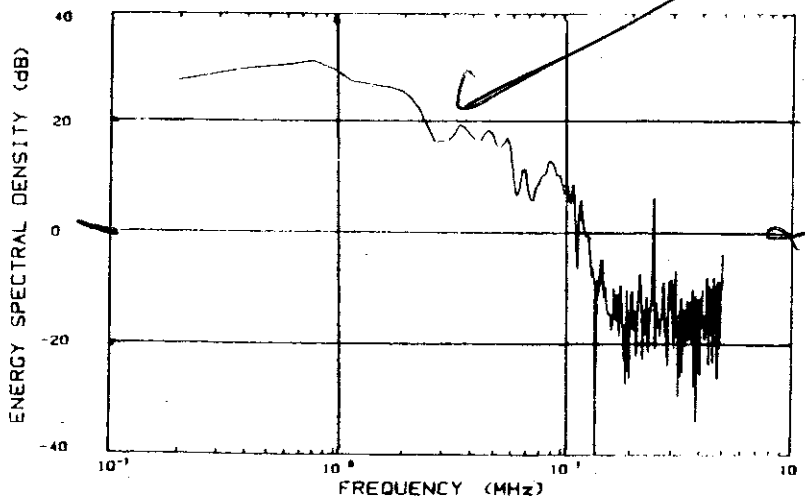
# RF TEST FREQUENCY RANGE LIGHTNING PULSE SPECTRAL DISTRIBUTION

ELECTRIC FIELD SPECTRUM



## SPECTRAL DISTRIBUTION for LIGHTNING CURRENT (I)<sup>2</sup> – DETERMINES INTERNAL MAGNETIC FIELDS

ELECTRIC-FIELD-DERIVATIVE SPECTRUM

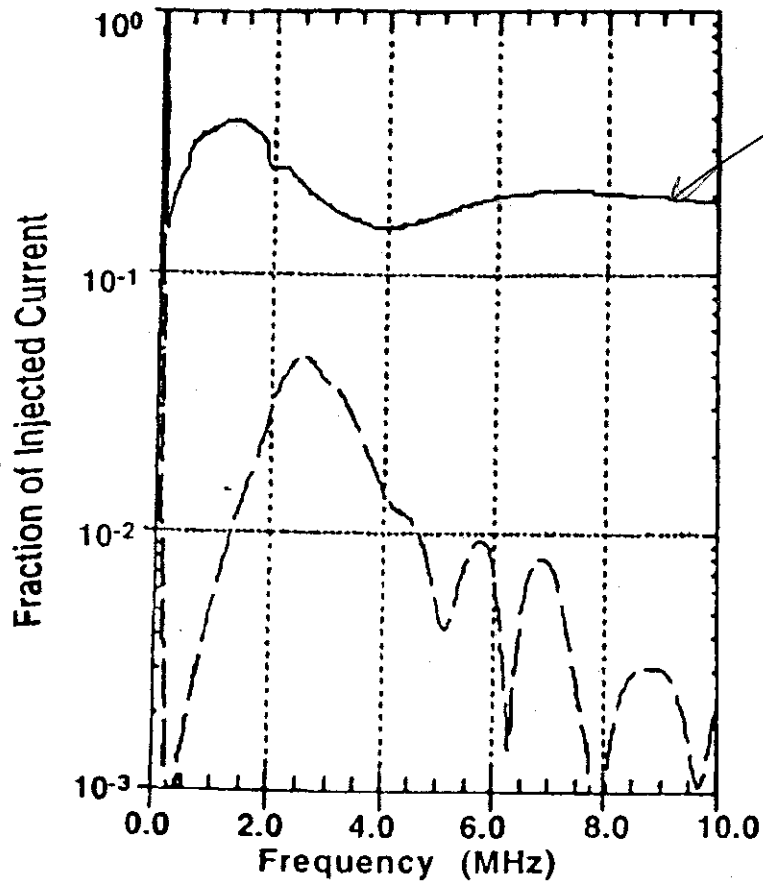


## SPECTRAL DISTRIBUTION for CURRENT DERIVATIVE (dI/dt)<sup>2</sup> – DETERMINES INTERNAL ELECTRIC FIELDS

FROM: "Lightning Electromagnetic Radiation Field Spectra in the Interval From 0.2 to 20 MHz", J. C. Willett, et al, Journal of Geophysical Research Vol. 95 D12 pp. 20,367 – 20, 387 Nov. 20, 1990  
(Graphs for a typical first return stroke, Fig A1; I is approximately proportional to external Electric Field)

**RESIDUAL HAZARD - CURRENTS ON BONDED PENETRATIONS:**

**RF PENETRATION TESTING (CONTINUED):**



**EXAMPLE RF PENETRATION TEST RESULTS FOR A VENT STACK BONDED TO A CONCRETE REBAR STRUCTURE**

**SOLID LINE - CURRENT ON VENT STACK EXTERIOR**  
**DASHED LINE - CURRENT ON VENT STACK INTERIOR**  
**(CURRENTS EXPRESSED AS FRACTIONS OF THE RF INJECTION CURRENT ON THE LPS)**

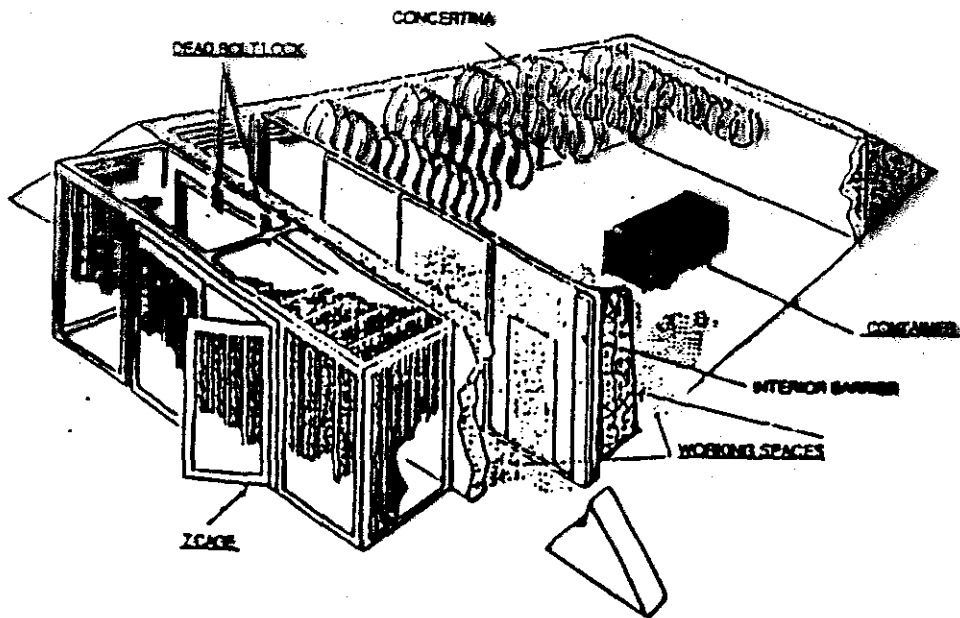


Figure B.2 Earth Covered Storage Igloo -- Lightning Strike Model

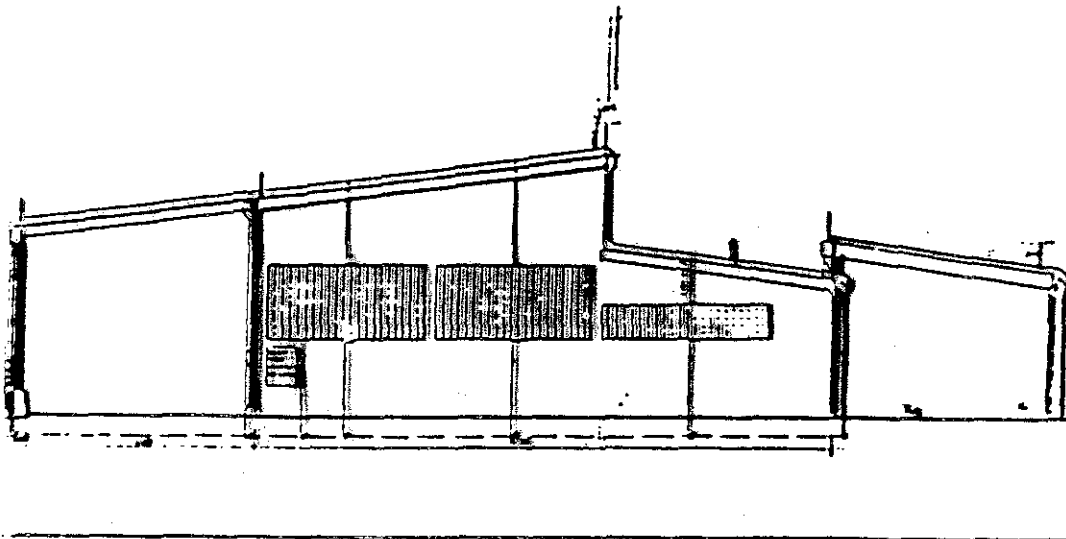
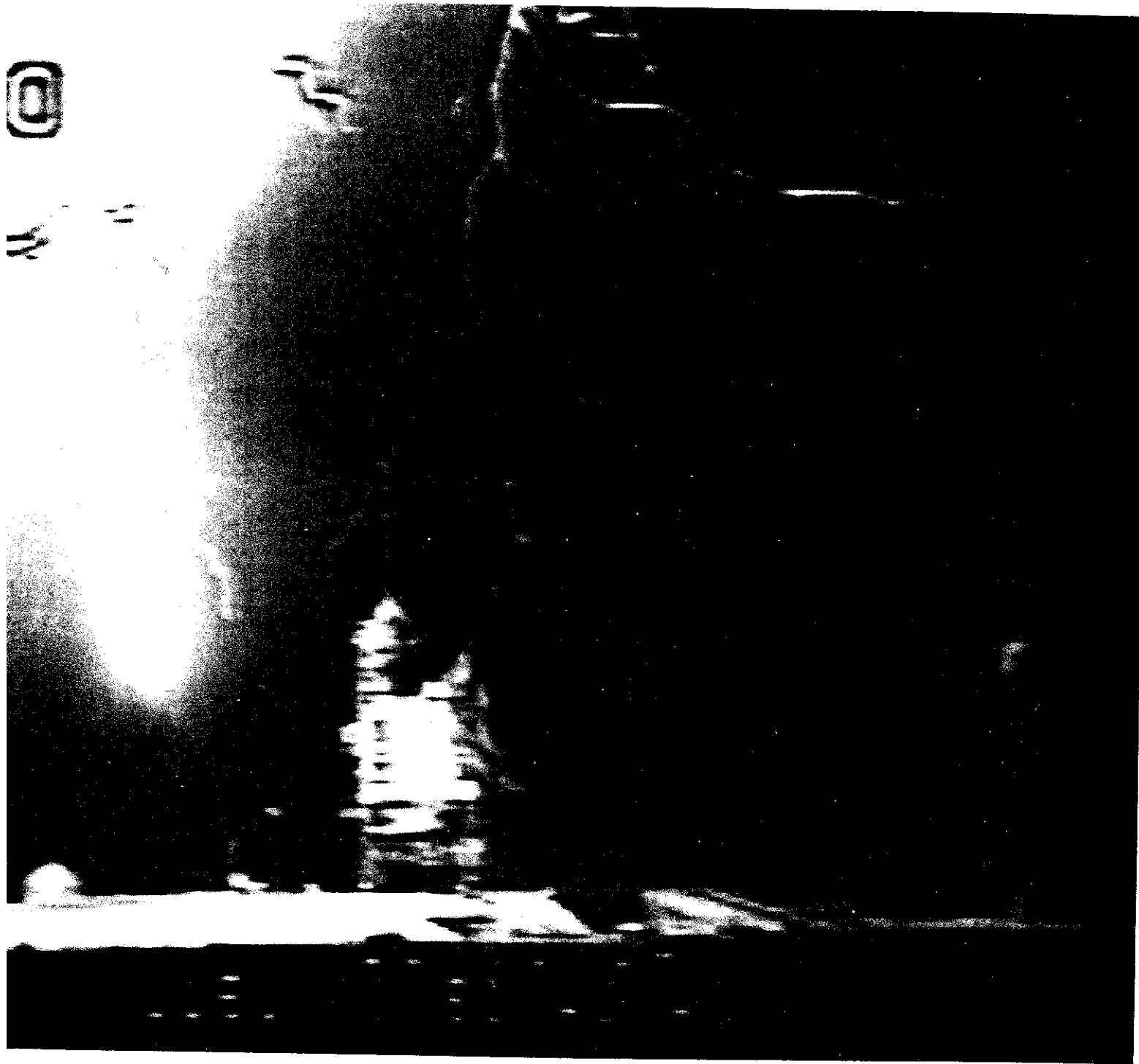


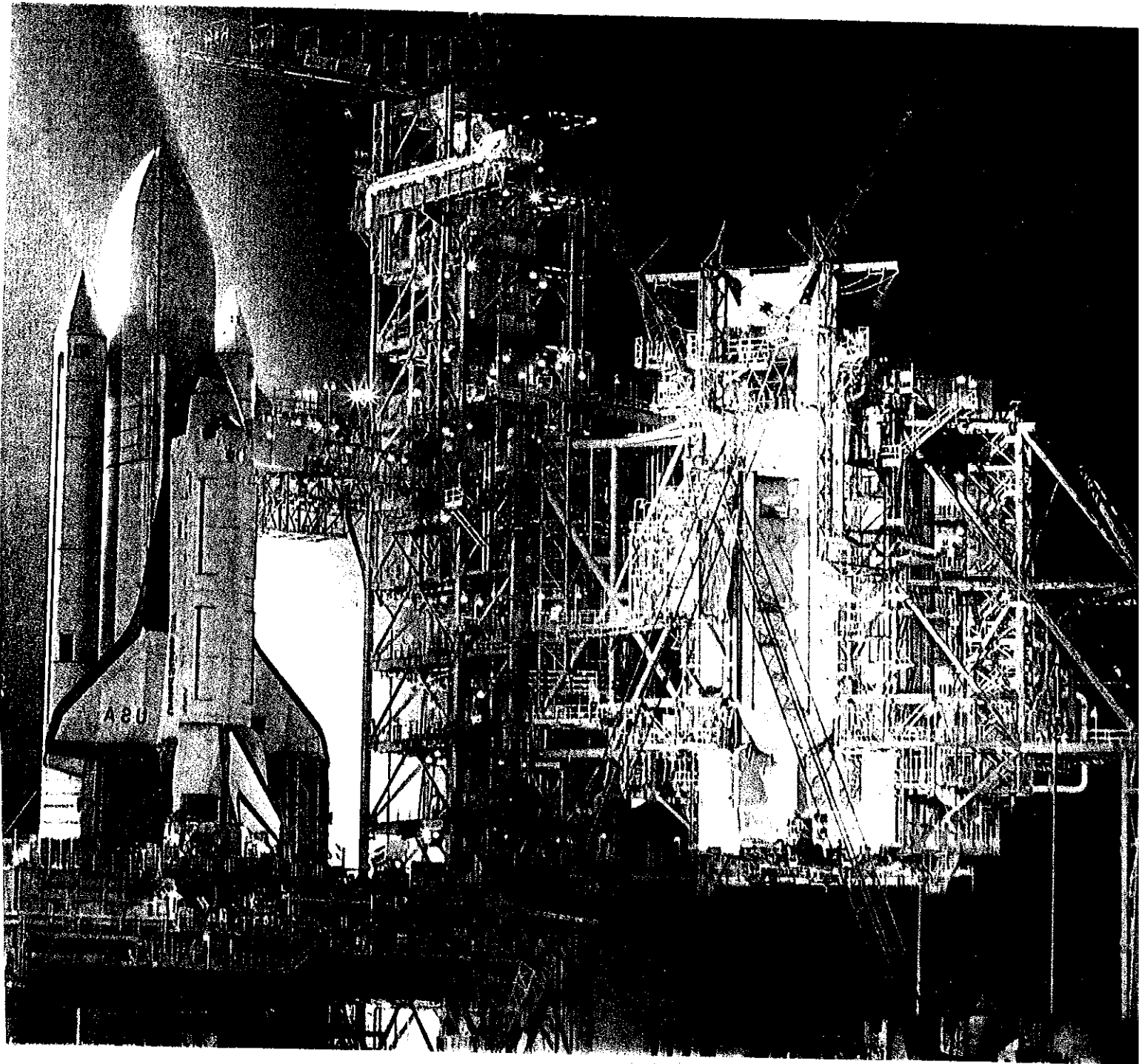
Figure B.3 Building - Right Side View With Window Screens and Lightning Protection System

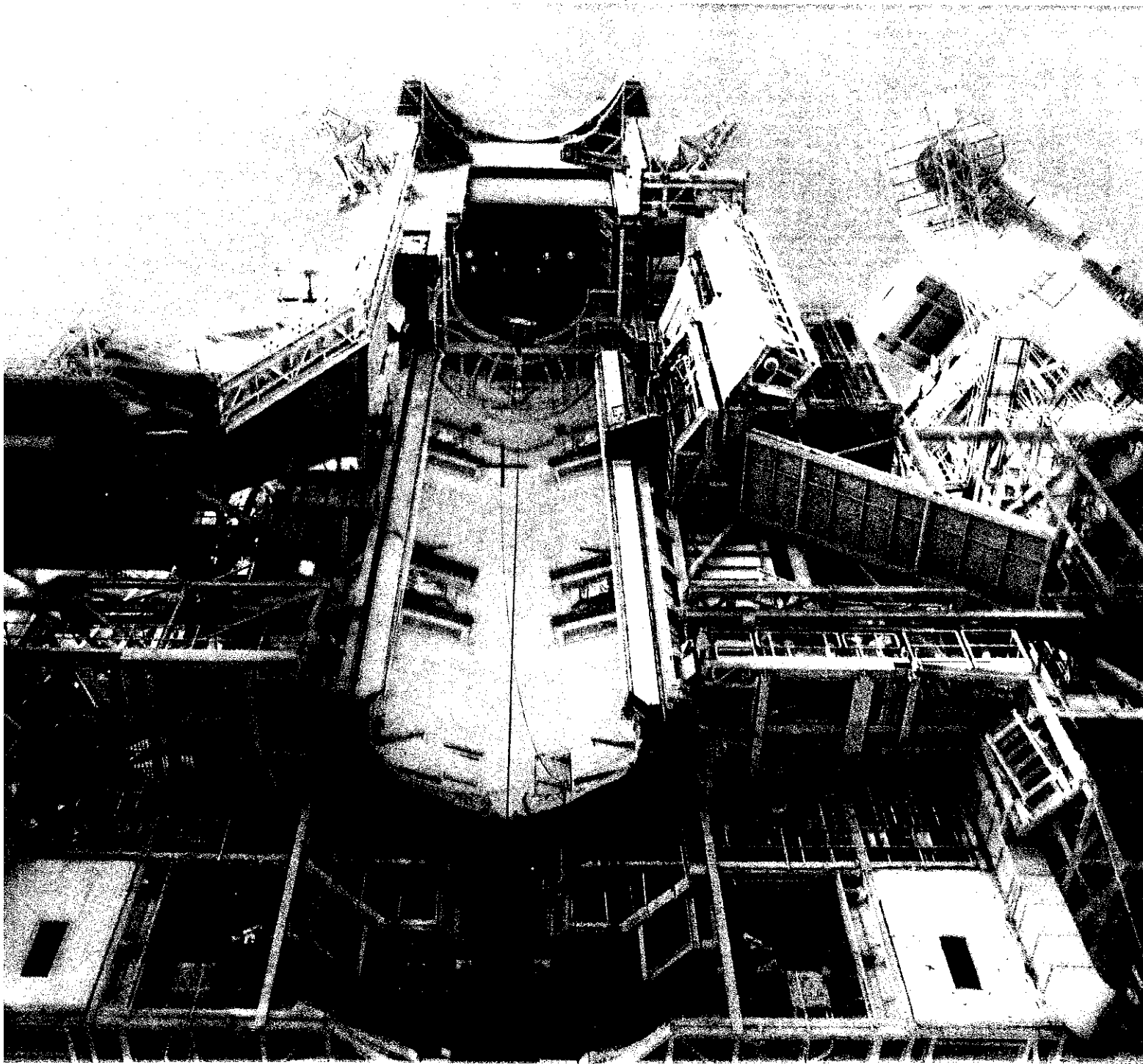


**Figure 4.1 Spent Rockets and Launchers for Triggered Lightning Experiments**









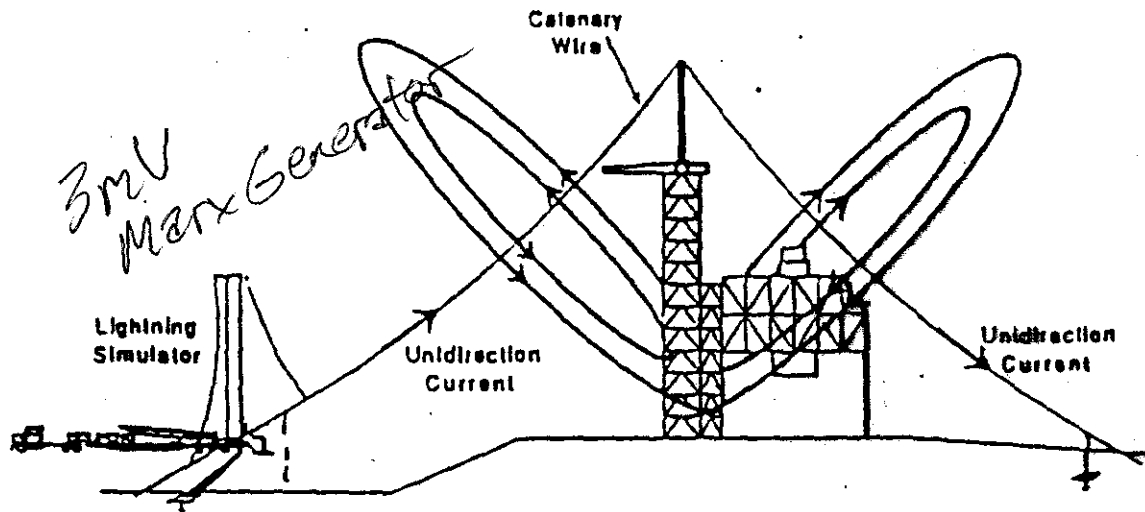


Figure 2. Test Configuration

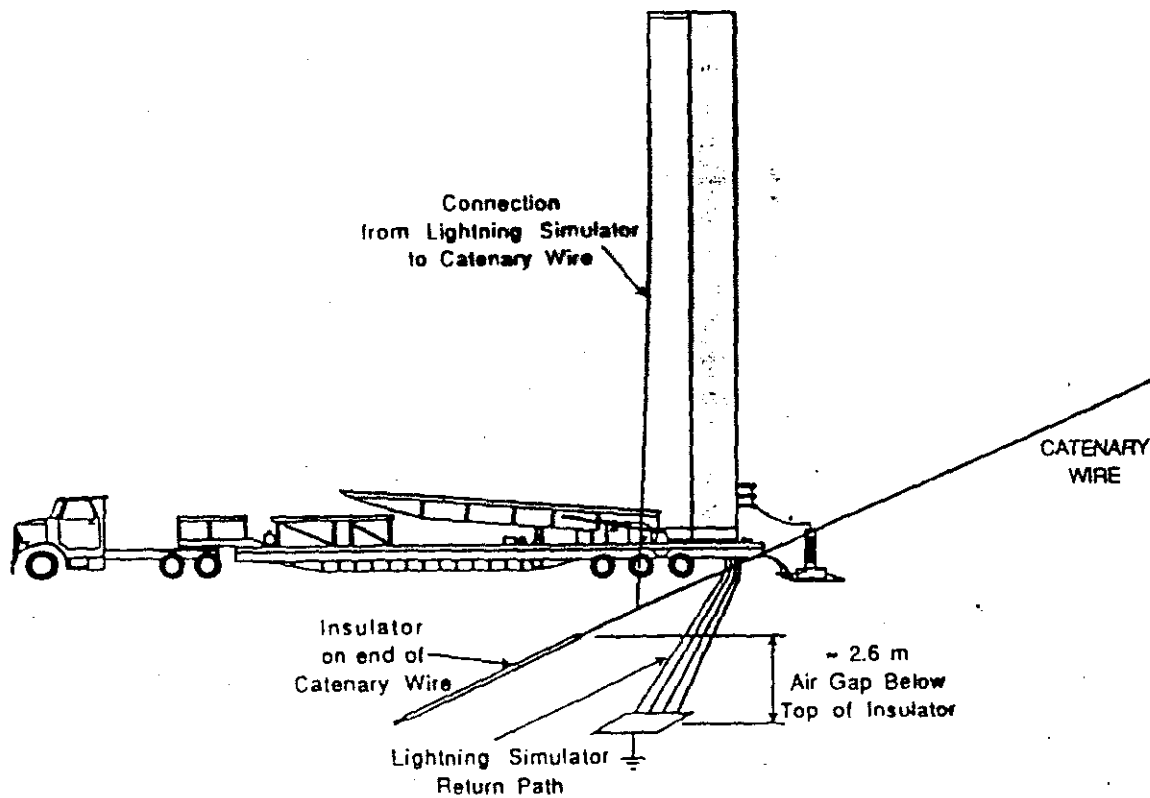
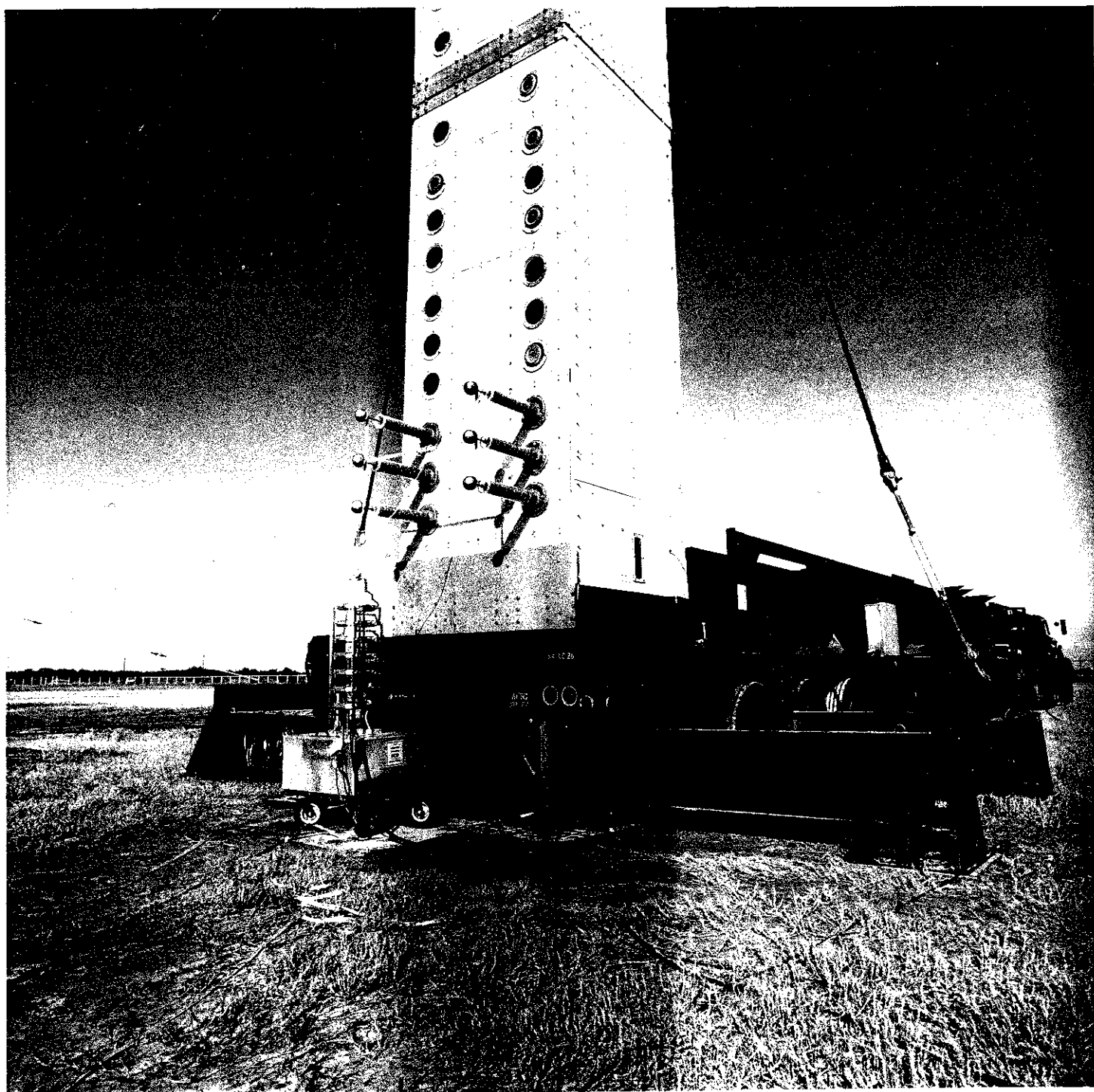
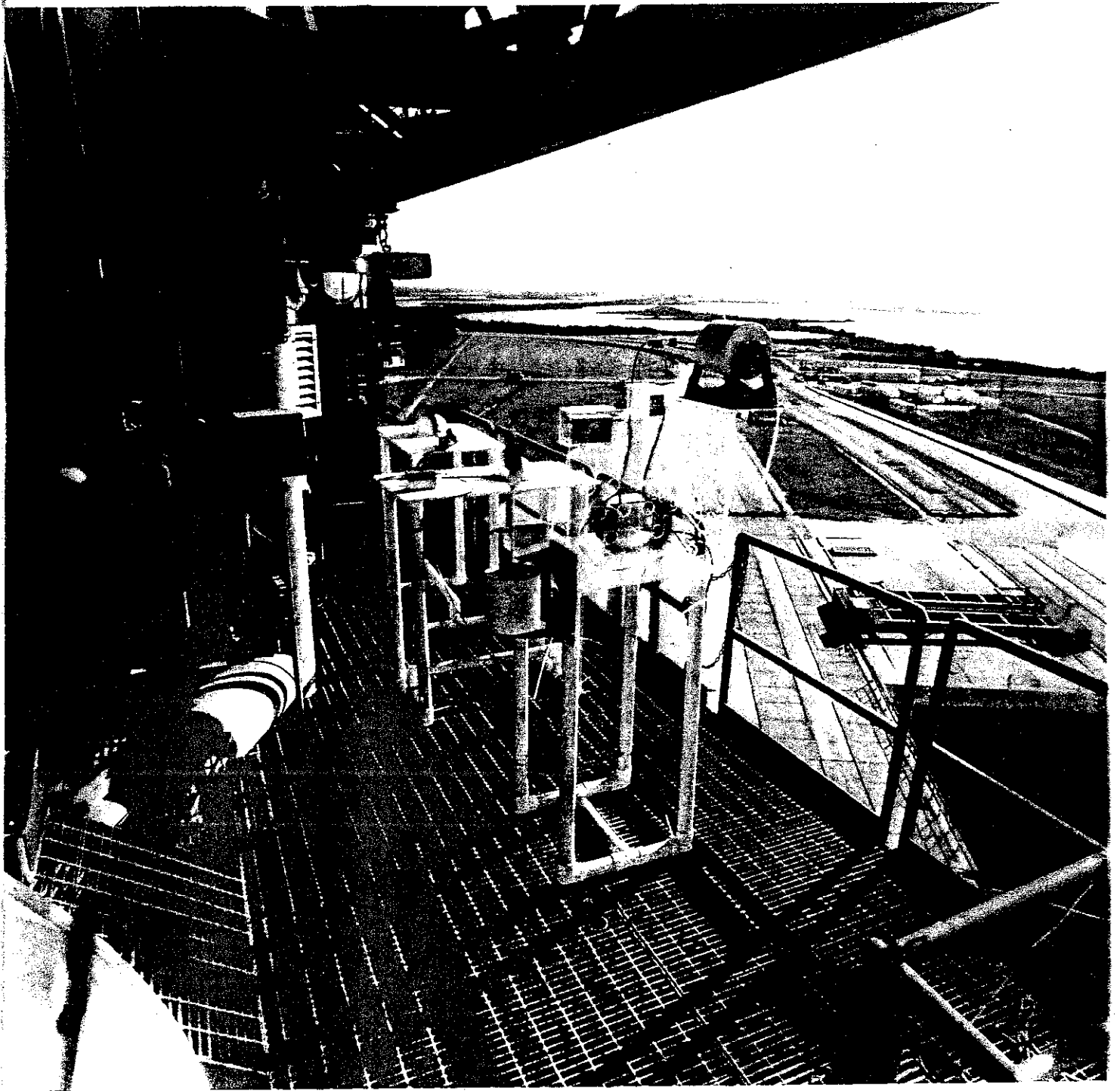
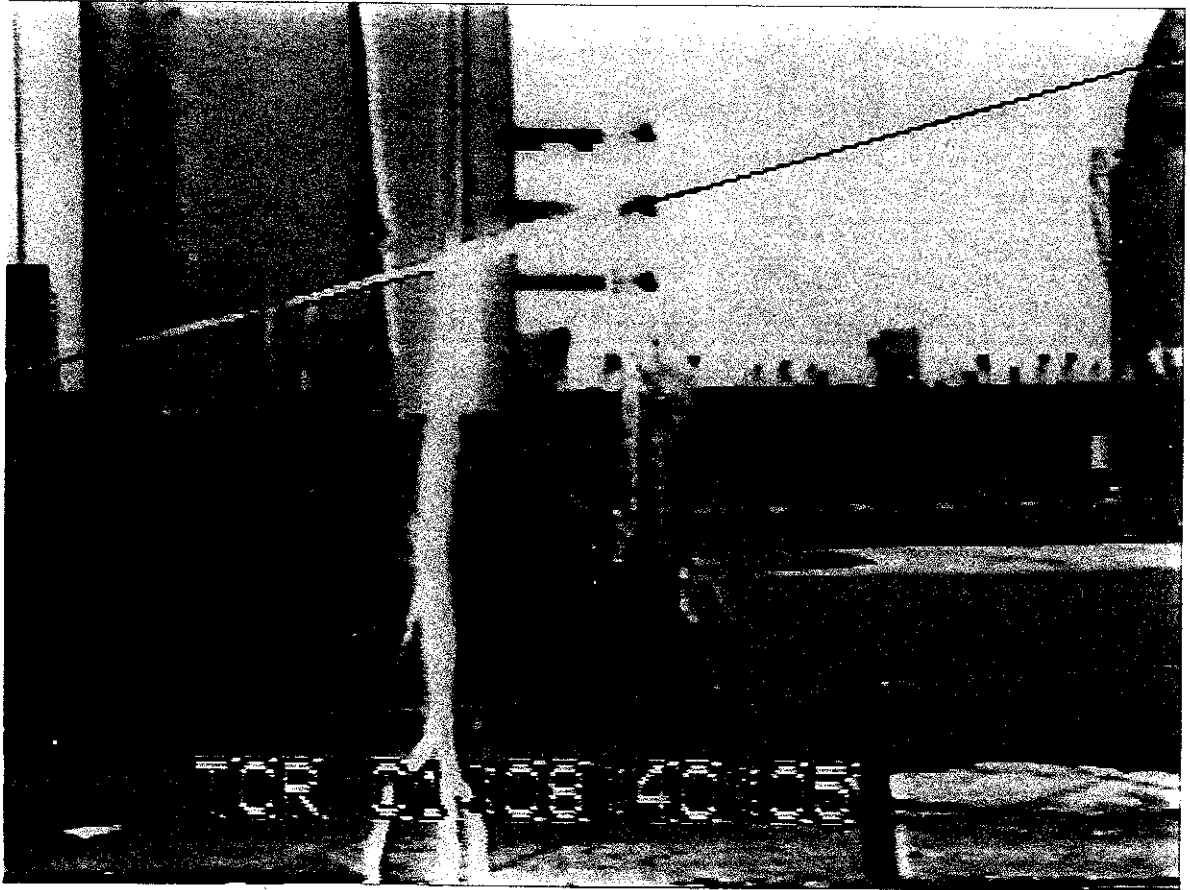


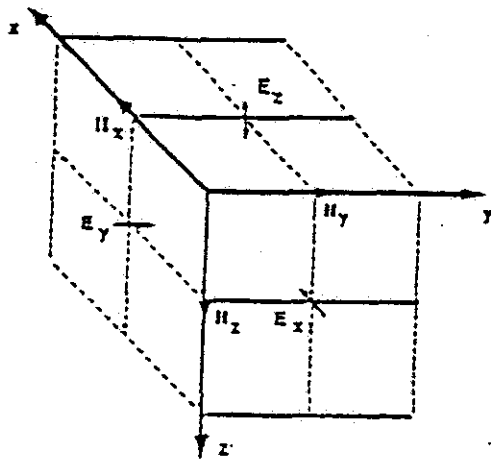
Figure 4-1. Simulator--Catenary Wire Configuration







The field components in each cell are calculated numerically via the finite difference form of Maxwell's Equations [3].



### MAXWELL'S EQUATIONS

$$\mu \frac{\partial \mathbf{H}}{\partial t} + \nabla \times \mathbf{E} = \mathbf{M} \quad (2.1)$$

$$\epsilon \frac{\partial \mathbf{E}}{\partial t} + \sigma \mathbf{E} - \nabla \times \mathbf{H} = -\mathbf{J} \quad (2.2)$$

$$\nabla \cdot \mathbf{E} = \frac{\rho}{\epsilon} \quad (2.3)$$

$$\nabla \cdot \mathbf{H} = 0 \quad (2.4)$$

Figure 2.1 Staggered Spatial Grid

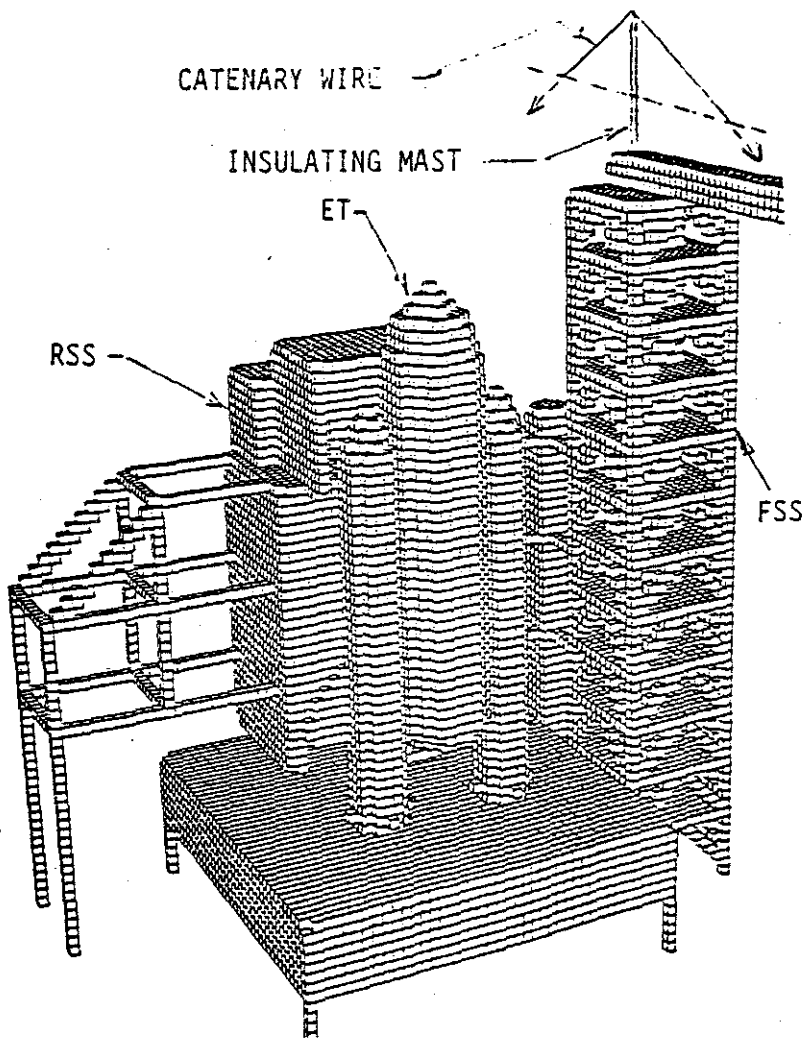
The vector components of equations 2.1 and 2.2 describing the time advance of magnetic and electric fields respectively are shown in Figure 2.2 together with the centered finite difference formulation of these equations. It is seen that besides being staggered in space, the electric and magnetic fields are also staggered in time. The numbers MX, MY and MZ are the numbers of cells in the X, Y and Z directions respectively.

The time step (increment) for this finite difference solution of Maxwell's Equations is determined by the Courant criterion, which may be viewed as requiring that the speed of numerical propagation be greater than the fastest physical wave speed, in this case the speed of light in air. Specifically, the Courant condition is:

$$\Delta t \leq \frac{1}{c \sqrt{\frac{1}{\Delta x^2} + \frac{1}{\Delta y^2} + \frac{1}{\Delta z^2}}} \quad (2.5)$$

where  $\Delta t$  is the time step,  $\Delta x$ ,  $\Delta y$ , and  $\Delta z$  are the three cartesian spatial increments and  $c$  is the speed of light in the air. For the external coupling problem  $\Delta t$  is  $1.8 \times 10^{-9}$  sec and for the internal coupling problems  $\Delta t$  is  $.9 \times 10^{-9}$  sec. The smallest spatial increments control the time





(a) LAUNCH PAD OVERVIEW

(b) CUTAWAY SHOWING ORBITER

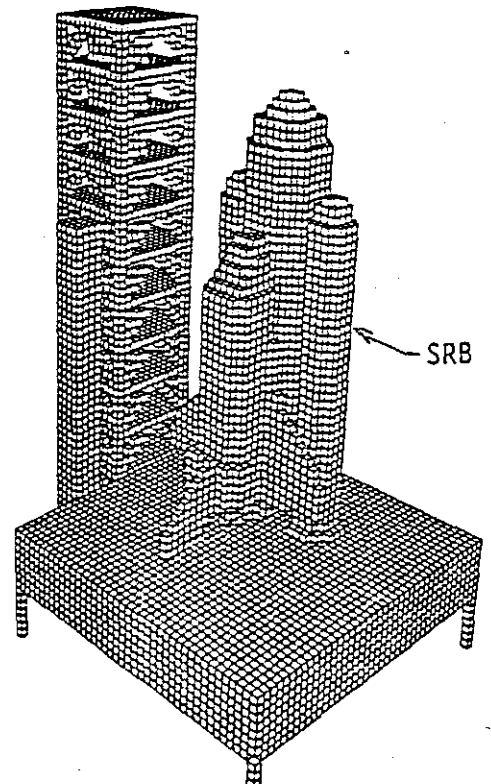
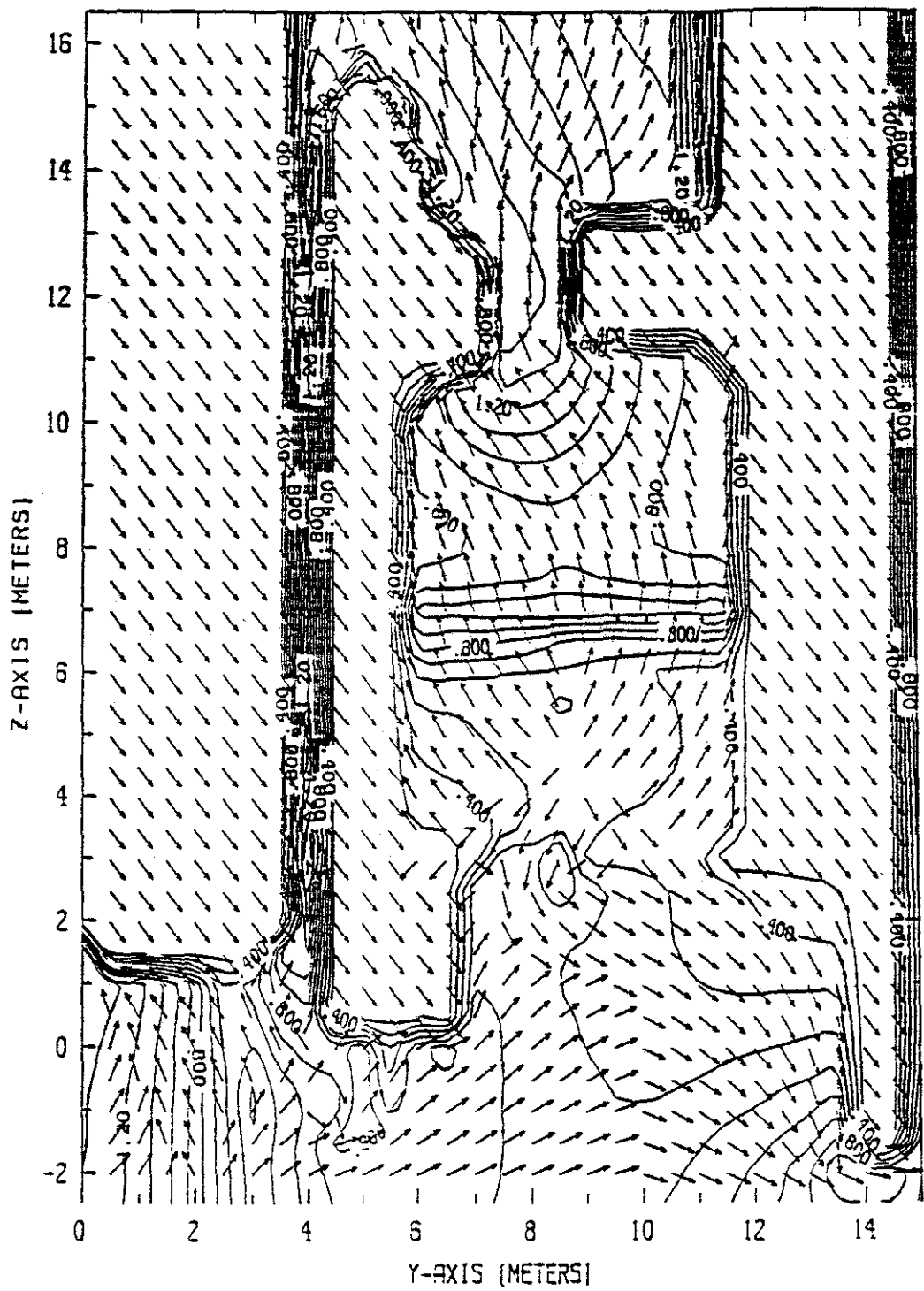


FIGURE 1. DIAGRAM OF THE ELEMENTS OF THE LAUNCH PAD STRUCTURE AS THEY HAVE BEEN MODELED

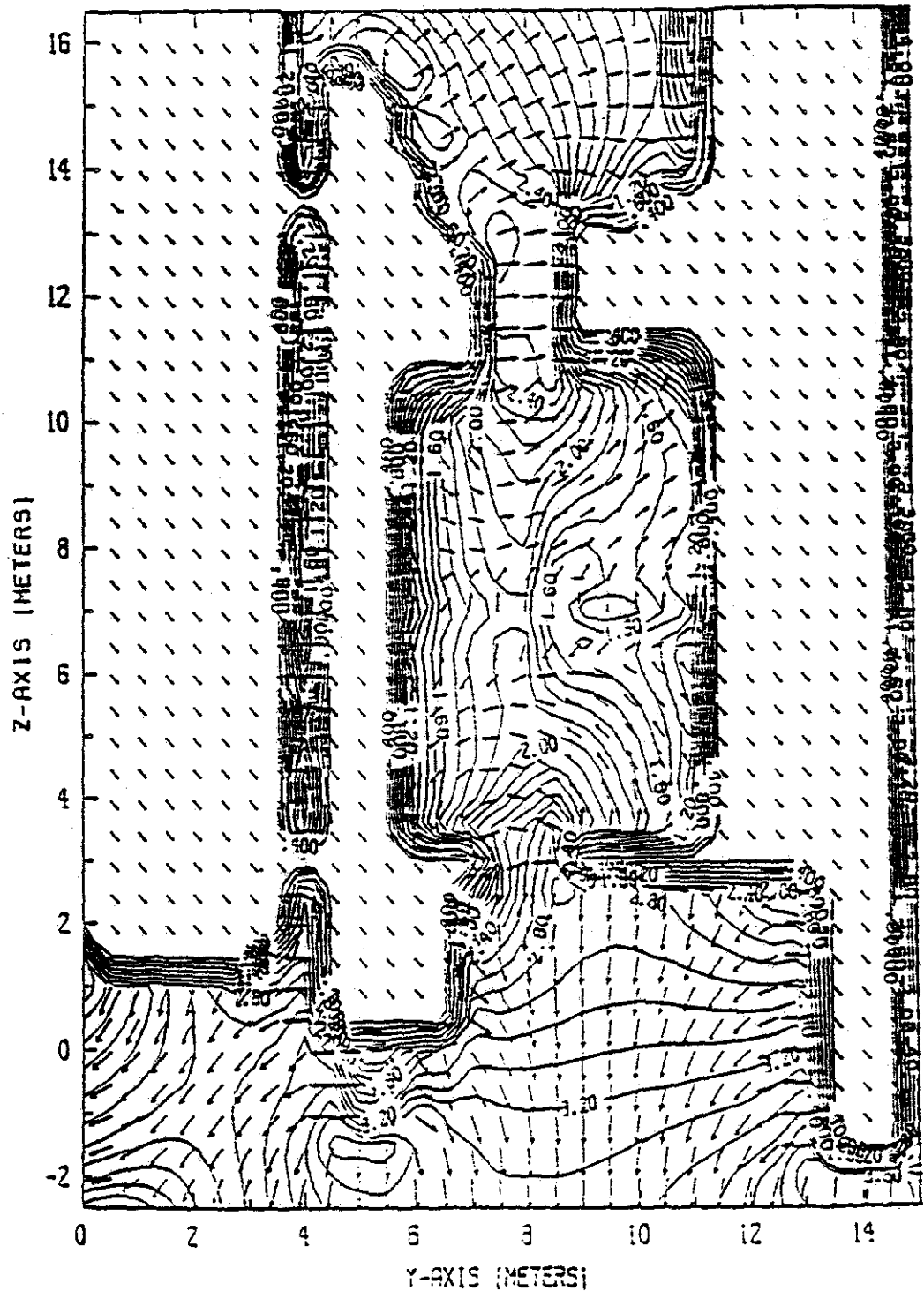


$\log_{10}(H)$  (H in A/M)

CFW11: I=(H+1)

FIELDS AFTER 720 NSEC

H-FIELD CONTOURS ON A VERTICAL CROSS SECTION OF PCR AND SHUTTLE

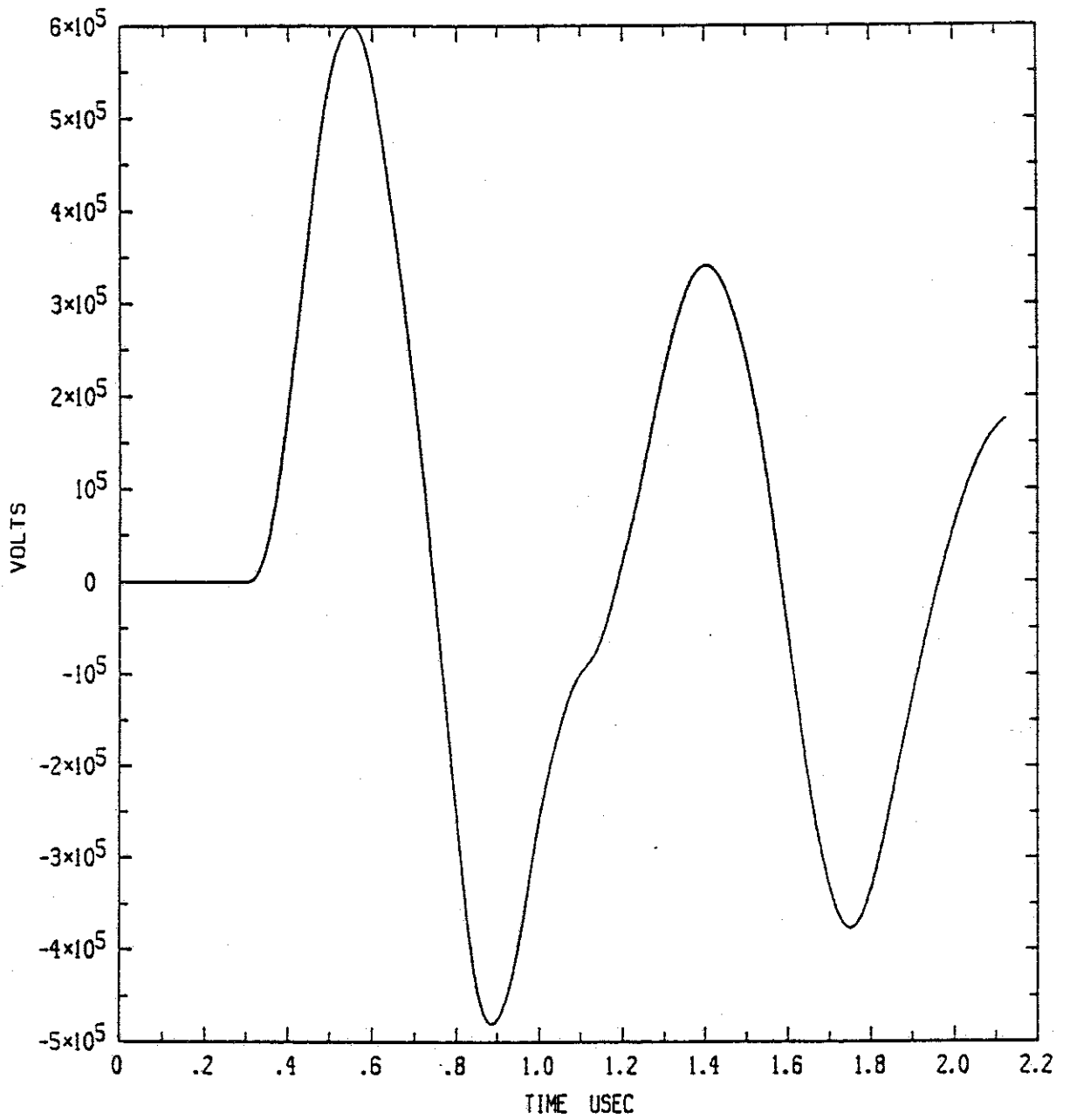


$\log_{10}(E)$   $E$  in V/M

DFW11: I=IH-11

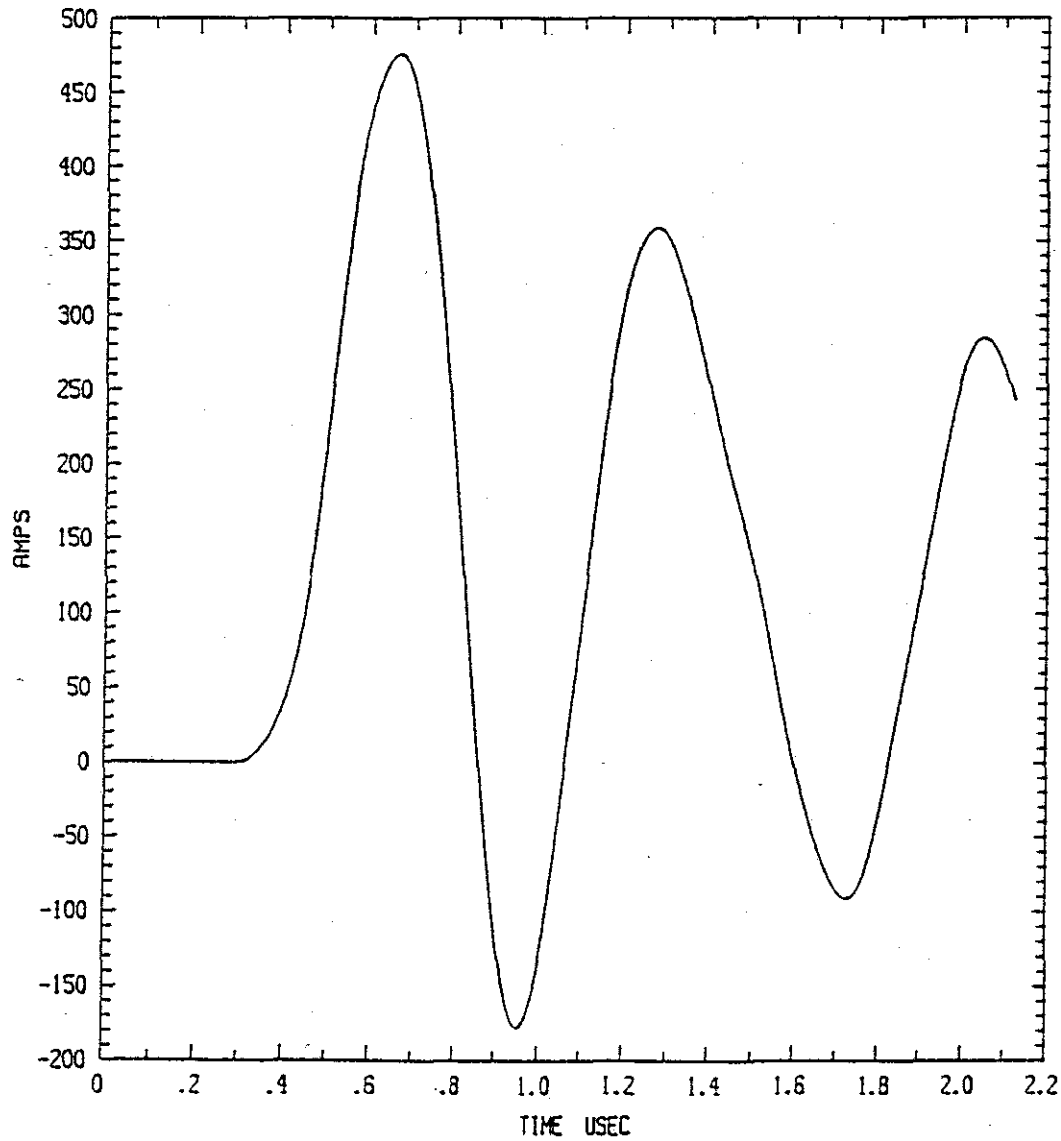
FIELDS AFTER 720 NSEC

E-FIELD CONTOURS ON A VERTICAL CROSS SECTION OF PCB AND SHUTTLE



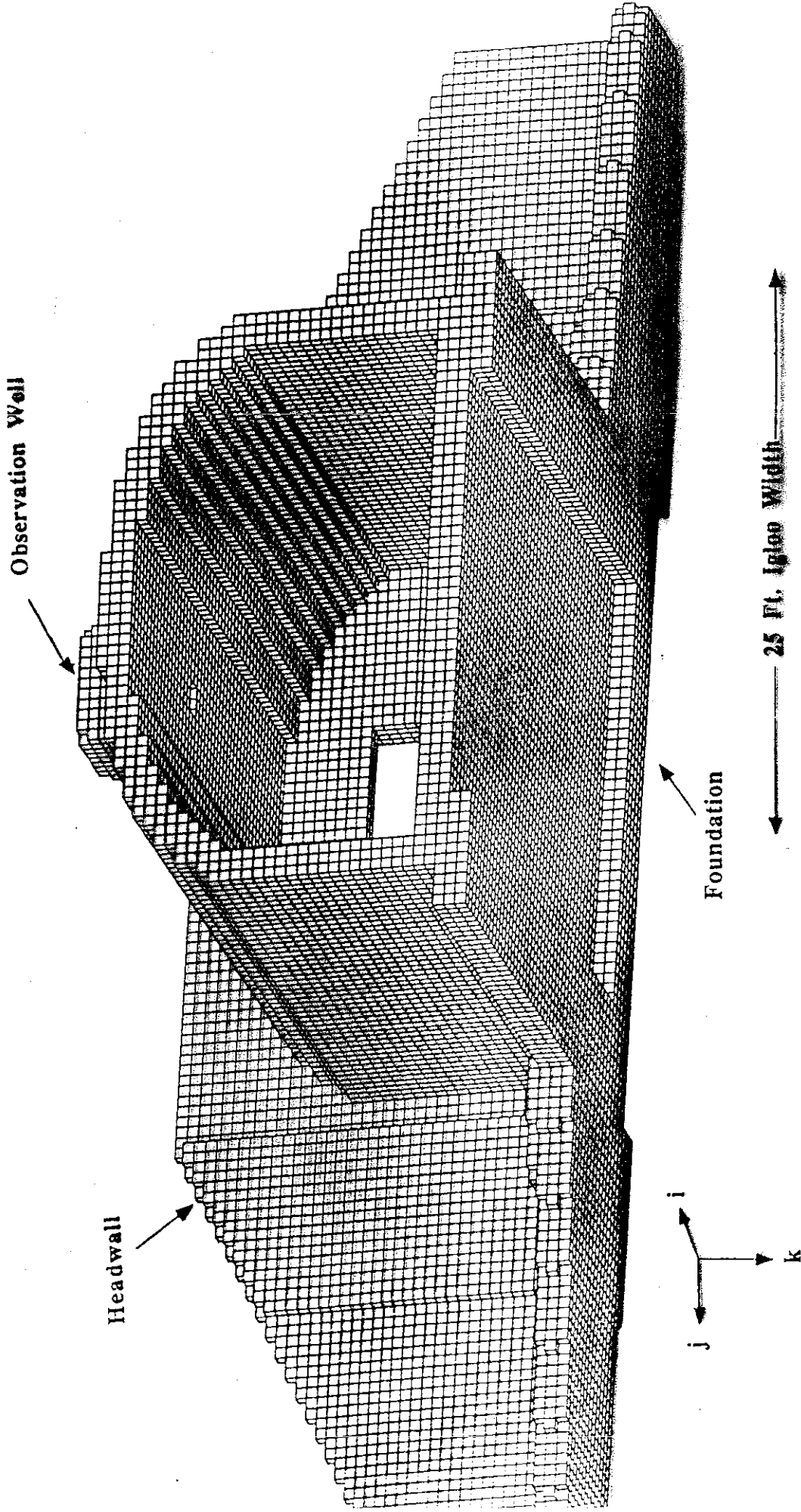
OPEN CIRCUIT VOLTAGE  
FROM INSIDE SHUTTLE PAYLOAD BAY  
TO INSIDE WALL OF PCR  
DATA RUN: D01  
LIGHTNING STRIKE TO TOP OF LIQUID FUEL TANK

Figure 4.5. Resonant Response of the PCR/FSS/RSS/Shuttle System from an Attachment to the Catenary Wire



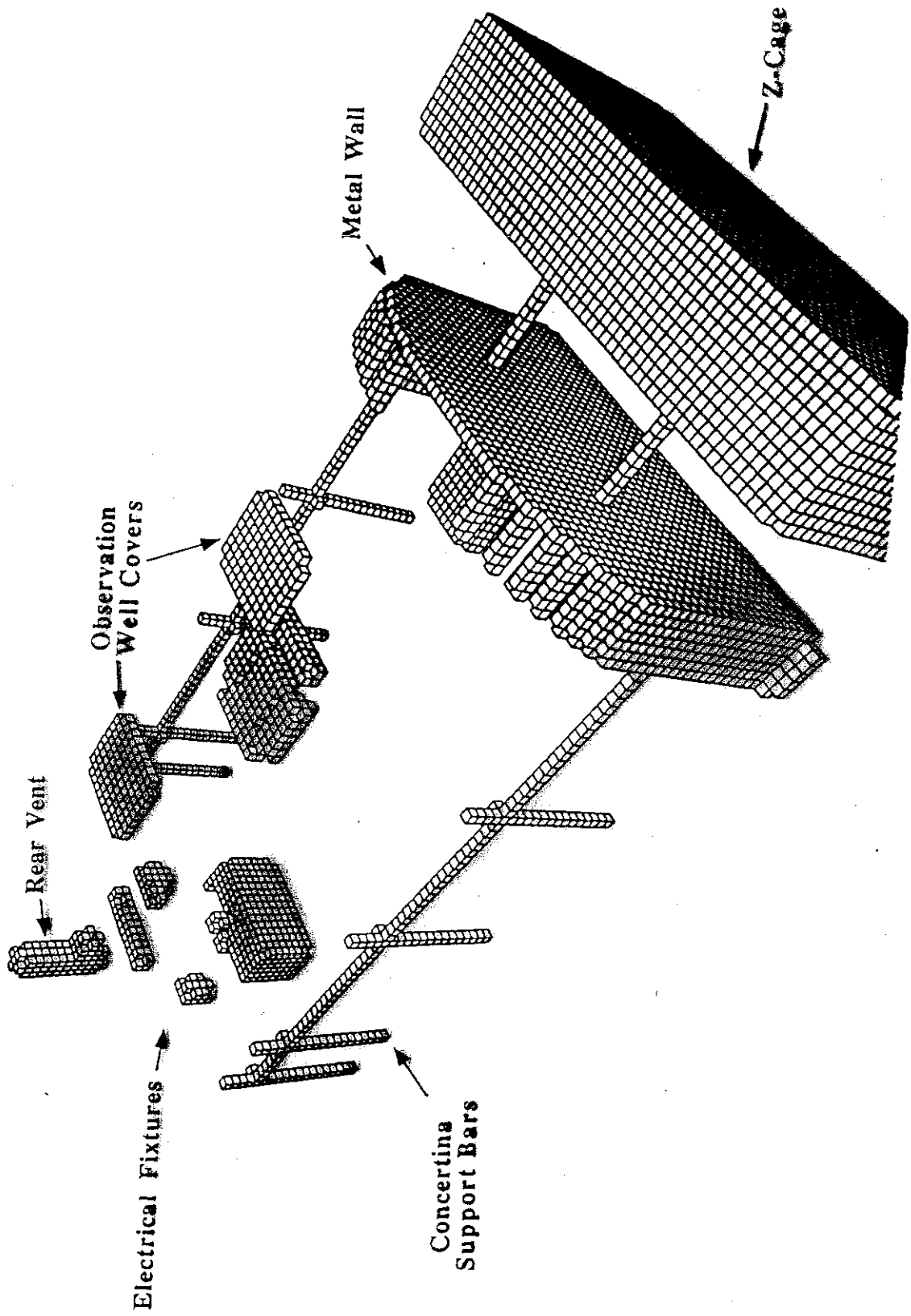
SHORT CIRCUIT CURRENT  
FROM SHUTTLE FUSELAGE TO WALL OF PCR  
ON ONE OF THE FOUR GROUNDING STRAPS  
DATA RUN: W01  
LIGHTNING STRIKE TO TOP OF CATENARY CABLES

# IGLOO CONCRETE

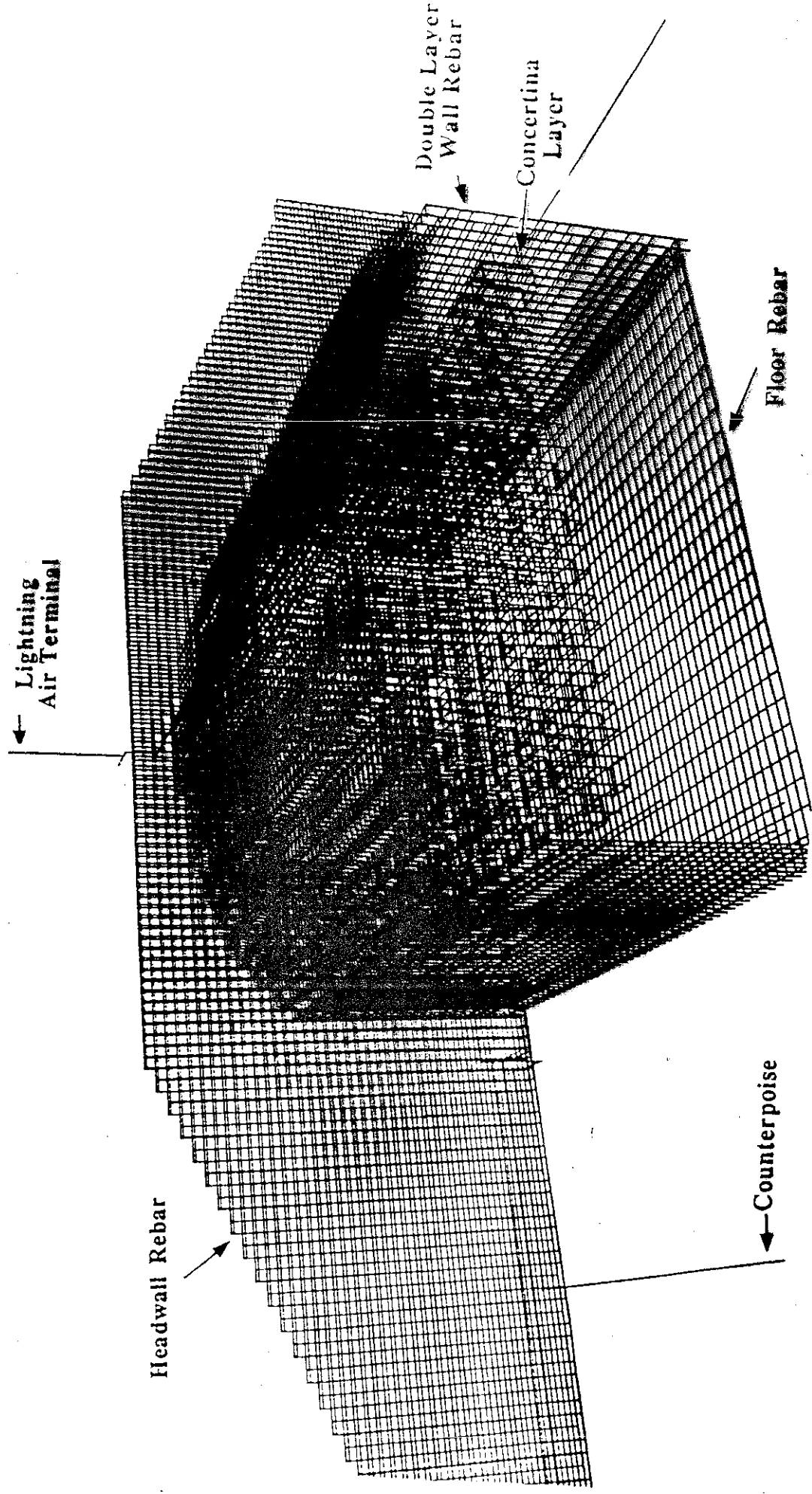


Single Cell Size  
8" x 6" x 6"

# IGLOO METALS



# IGLOO REBAR AND WIRING





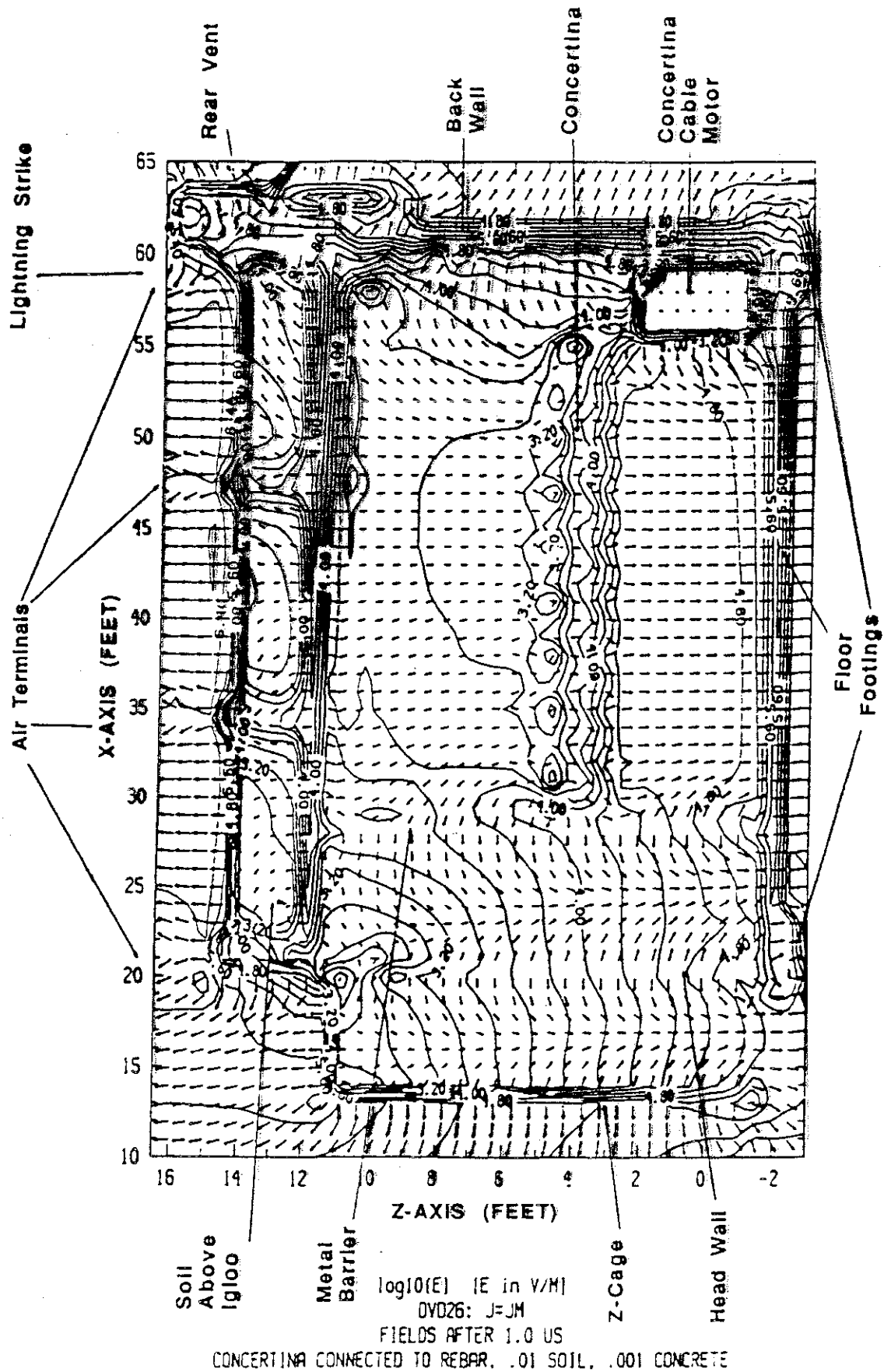
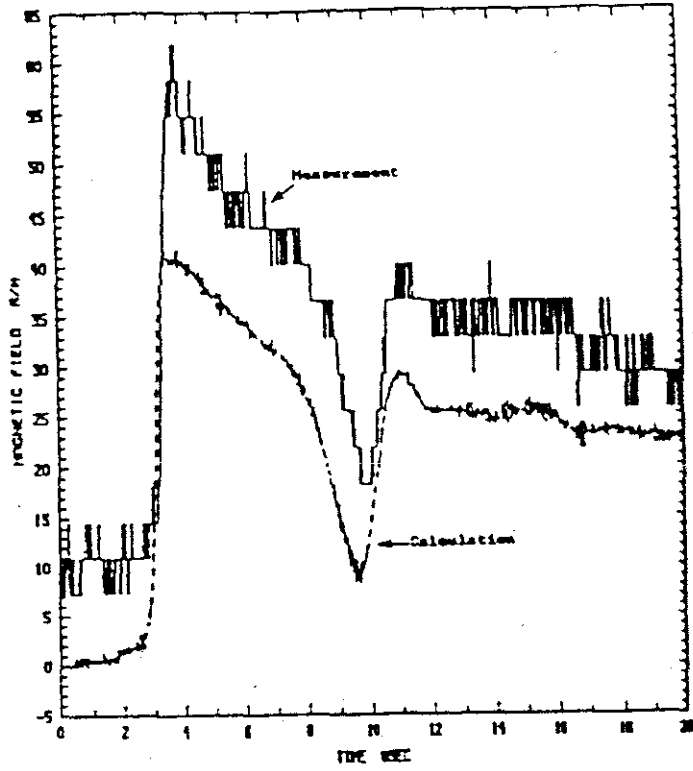
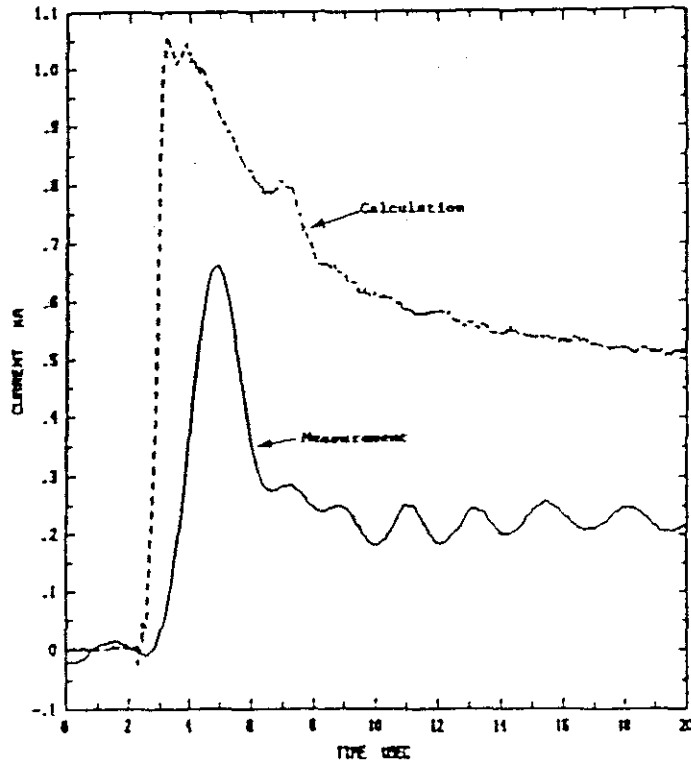


Figure B.8 Electric Field Vector and Magnitude Contour Plot for Vertical Mid-Cross Section of Igloo



(e) Internal Magnetic Field in Vicinity of Right Rear Corner of Igloo



(f) Current on Conductor Between Z-Cage and Counter-Poise

Figure 4.9 (Cont'd.) Comparison of Analysis with Experimental Results for Partially Buried Concr [7, 8] Igloo Rocket Triggered Lightning Experiment Picatinny Arsenal/Sandia Laboratories